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## A 30-KV PROTON INJECTOR FOR PIGMI\*

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### Summary

A 30-kV proton injector designed for matching a 31-mA proton beam into the radio-frequency quadrupole (RFQ) section of the PIGMI accelerator has been constructed and tested. This injector uses a small, efficient duoplasmatron ion source and a single-gap extraction system for creating a convergent ion beam, and a three-element unipotential lens for focusing the ion beam into the RFQ. A description of this prototype injector is presented, along with the experimental data obtained during the testing of this system.

### Introduction

Under the PIGMI (Proto-Generator for Medical Irradiation) program at the Los Alamos National Laboratory, the major techniques for constructing a compact linear accelerator for proton therapy have been identified and developed<sup>1</sup> and the construction of this accelerator has been described.<sup>2</sup> The PIGMI accelerator begins with a compact RFQ injector, followed by an RFQ linac.

The RFQ linac greatly simplifies the low-energy end of the accelerator. It can accept a bunched proton beam from the injector and accelerate it to 16 MeV in 1.7 m, at which point the beam is easily injected into the conventional drift tube linac. In addition, the RFQ also provides beam capture of the unperturbed beam, as well as beam focusing. Thus, the RFQ has eliminated the need for a large, high-current electron gun, power supply, a complex multi-energy buncher system, an extensive low-energy beam transport system, and associated control instrumentation.

The 30-kV injector energy was chosen to minimize the length of the RFQ with the optimum capture efficiency, while allowing reliable operation of the single-gap beam-brightening extraction system. Injector operation at 30 kV dramatically simplifies the design and makes the system small while increasing its reliability. In addition, this low injector energy for the RFQ allows electrostatic focusing of the ions because it is more effective than magnetic focusing at this energy. Thus, a lens system can be used to match the 30-kV proton beam from the injector into the RFQ.

In the final experimental program, a prototype of this compact 30-kV injector has been constructed and tested. This injector contains a small, efficient duoplasmatron ion source, a single-gap extraction system, an einzel lens, and magnet-free equipment enclosed in a small, reentrant vacuum chamber that attaches directly to the vacuum housing of the RFQ. A self-contained equipment cabinet contains the electronics, power supplies, and other systems to operate the ion source, extraction system, vacuum system, and einzel lens.

### Injector Description

#### Duoplasmatron Ion Source

A new duoplasmatron ion source was constructed for this prototype injector. This small ion source uses the same filament, intermediate electrode, plasma aperture, and plasma-expansion-cup geometry as the previous PIGMI injector,<sup>2</sup> but has a smaller anode housing, a more compact and magnet-free, or a simpler, water-cooling system. The water cooling is maintained by channels cut into the copper housing for the arc magnet coil. The housing is brazed onto the intermediate electrode so that the coil is not exposed directly to the water. Magnetic field calculations were used to verify that the anode housing and arc magnet coil do not couple magnetic field between the intermediate electrode and anode at the point of the plasma exit, with only a small increase of the magnetic flux density. The final design for this source is shown in Fig. 1.

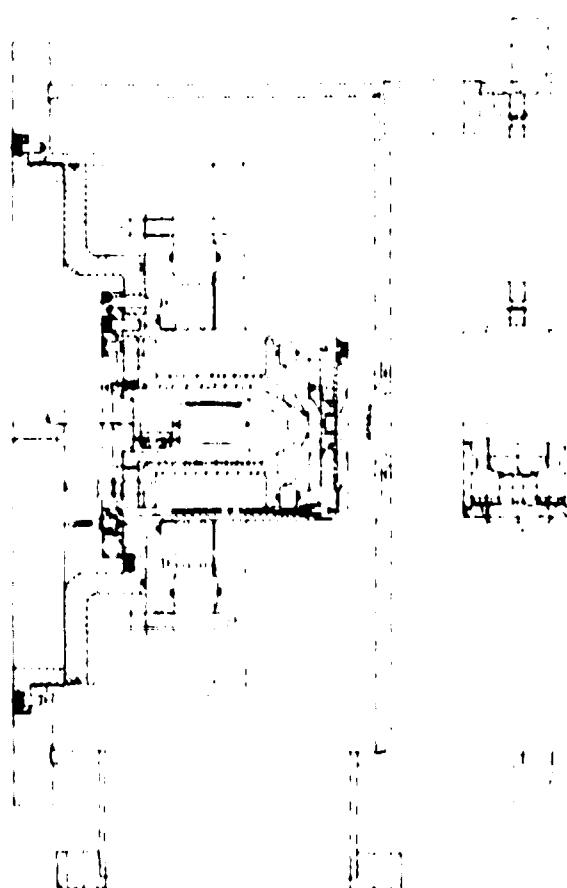


FIG. 1. Cutaway view of the 30-kV injector.

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The inner plasma-expansion cup in this duoplasmatron uses a boron nitride insulator along the straight side of the cup. This self-biasing electrode, suggested by Bacon<sup>3</sup> for this geometry, increases the proton fraction in the extracted ion beam to 95% or more, compared to the 70% this geometry yields without the insulator.<sup>4</sup>

#### Extraction System and Vacuum Housing

The cutaway view of the injector in Fig. 1 also shows the arrangement of the 90-kV extraction gap and high-voltage insulation of the ion source within the de-entrant vacuum housing. The high-voltage insulation is maintained by a single glass insulator held between two flange surfaces by permanent bolts. The radial alignment of the ion source is maintained by precision machined lips on each surface. The outside of the insulator and the permanent spacers are all boron-nitridized to prevent sputtering of the insulator during the electron-beam annealing process.

As shown in Fig. 1, the ion source extraction gap is located at the center of the 90-kV extraction gap. The two outer electrodes of the extraction gap are connected with the ion extraction electrode. The outer electrodes are connected to the ground plane of the 90-kV extraction gap. The outer electrodes are connected to the ground plane of the 90-kV extraction gap. The outer electrodes are connected to the ground plane of the 90-kV extraction gap. The outer electrodes are connected to the ground plane of the 90-kV extraction gap.

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#### Extraction System Options

In addition to providing the standard 90-kV extraction system, the injector can be supplied with an optional 100-kV extraction system. This system consists of three additional electrodes inserted between the outer electrodes of the 90-kV extraction gap and the ion source. The outer electrodes of the 90-kV extraction gap are connected to the ground plane of the extraction gap. The outer electrodes of the 90-kV extraction gap are connected to the ground plane of the extraction gap. The outer electrodes of the 90-kV extraction gap are connected to the ground plane of the extraction gap. The outer electrodes of the 90-kV extraction gap are connected to the ground plane of the extraction gap.

space has been used for insertion of beam diagnostics equipment. A biased beam stop and a multiwire beam harp can be individually inserted to measure the extracted ion current or beam profile. In addition, a small window-frame steering magnet can be inserted to magnetically steer the extracted ion beam through the einzel lens and into the RFQ. This steering can be used to compensate for small misalignments in the system.

#### Equipment Cabinet

The equipment cabinet, shown in Fig. 2 with the injector mounted, is a self-contained system for operating the injector. The entire high-voltage region of the injector has been enclosed in an interlocked, grounded cabinet (76 in. high by 24 in. wide by 41 in. deep). As seen in Fig. 2, the front half of the cabinet contains, from the bottom up, the turbomolecular pump power supply; the high-voltage power supply; the ion source power supplies located at high voltage; an oscilloscope for monitoring the arc pulse; the einzel-lens control and meter; the pulsing and timing controls for the injector system; and the ionization gauge controller. The rear portion of the cabinet contains the high-voltage isolation transformer rated for 100 kV, the hydrogen gas bottle regulator and gas distribution system, the gas detector tube assembly, the high-voltage crowbar system, the energy loss power supply, and the cold stage of the system for the ion source. An interlocked double door allows easy access to the front half of the cabinet, and thus to the base of the injector, and the associated power supplies, the high-voltage transformer, and the gas system. All of the components in the front portion of the cabinet are grounded. In addition, the panel of the front half of the cabinet can be removed and the front of the injector can easily be accessed through the open cavity of the panel within the cabinet.

After removal of the power-supply panel, the power-supply units are located at high voltage, the main switch for the power supply, as well as the stepping motor for computer control, are located at high potential with insulated shafts to the front panel. All units for the power supply are located at high voltage, but are visible through glass windows on the front panel of the cabinet. The oscilloscope and current transformer used to monitor the arc pulse are at ground potential with the current lead from the arc pulse to the ion source isolated through the current transformer. The timing pulse for the traceless arc pulse and power-supply is supplied



Fig. 2. Cutaway view of beam optics for the 100-kV injector, including the einzel lens.

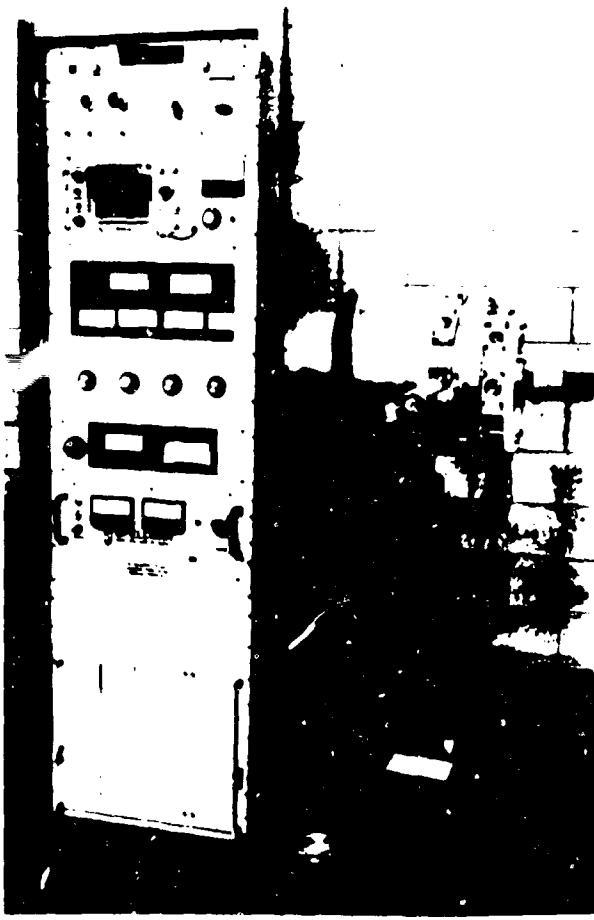


Fig. 3. The 30-kV injector and equipment cabinet.

from the master timer at ground potential through a fiber optics link. Space has been left in the injector high voltage region for a microprocessor to monitor the ion source power supplies and provide the information to the control system for the accelerator through another fiber optics link.

The high voltage in the cabinet is supplied by a rack mounted power supply located just below the high voltage region. The high voltage for the einzel lens is supplied by a small potted high voltage power supply controlled by a Variac. The high voltage isolator transformer is mounted on the rear floor of the cabinet. The hydrogen gas bottle also is mounted on the rear floor of the cabinet at ground potential, with the high pressure gas (100 psi) fed from the regulator to the hydrogen flow system in the high voltage region through PV tubing. The closed cycle water system for the ion source is located on the rear floor of the high voltage region in the cabinet; the water system contains a submersible vane pump mounted to a 10-l water reservoir, and a small automotive heater radiator mounted on a bracket frame below the exhaust fan located in the top of the equipment cabinet.

### Experimental Results

The prototype 30-kV injector system has been assembled and successfully tested. The assembled system was tested as shown in Fig. 3, but with several additional diagnostics beam boxes, one which had a 120-l/s turbomolecular pump attached to it. For these tests the typical operating parameters were

Arc voltage	120 V
Arc current	15 to 20 A
Arc magnet current	0.9 A
Filament current	30 A
Hydrogen gas flow	1.0 atm cc/min
Arc chamber pressure	180 microns
Column pressure	$6 \times 10^{-6}$ torr
Einzel lens voltage	0 to 32 kV

The injector was operated at 60 Hz, with a 75- $\mu$ s pulse width; it produced a 25-mA ion beam with a 31-kV extraction voltage. The extracted current increased to 30 mA at 33 kV, indicating that the extraction gap must be shortened to obtain the required 31 mA of protons at 30 kV.

During testing of the injector, an emittance measuring station was positioned with the slits at the same position as the RFQ entrance would be during accelerator operation. Emittance scans made at 31 keV, with an extracted beam current of 26 nA, gave a normalized emittance of 0.039 cm $\cdot$ rad for 96% of the beam. This is in excellent agreement with the normalized emittance of 0.037 cm $\cdot$ rad measured for this source, with a 26-mA beam at 11.5 keV, on the LAMPF ion-source test stand. Measurements on the test stand also showed that the proton fraction in the beam was 90%, and that the ion source could operate stably at a 1% duty factor.

The emittance measurements at 31 keV were made using the einzel lens; therefore, these measurements include the aberrations of the lens, a possible explanation for the small difference in the two measurements described above. However, these emittance measurements also showed that the einzel lens could be adjusted to produce a converging beam with the proper match for the RFQ, as shown in Fig. 4, where the acceptance of the RFQ, the experimental phase space of a 26-mA beam, and the calculated phase space for a 31-mA beam are overlaid on the same plot.

During magnetic field measurements it was found that the flux leakage into the plasma expansion cup of the new deplasmatron was almost double the value measured on the larger version of this source. This is probably from saturation caused by using a thinner and smaller iron anode housing; this is also suspected as the cause of the larger emittance from this ion source ( $>0.04$  cm $\cdot$ rad) relative to the emittance of the larger version of the ion source ( $0.03$  cm $\cdot$ rad). However, small changes in the anode aperture mounting arrangement could reduce the flux leakage and increase the brightness of this injector, if necessary for accelerator operation.

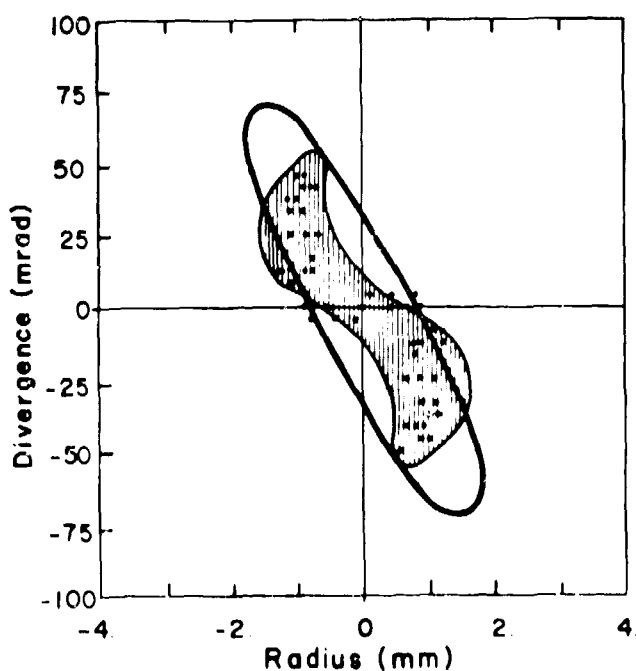


Fig. 4. Overlay of calculated (dots) and measured (vertical lined area) ion-beam phase space with the calculated acceptance (ellipse) for the RBU.

#### Acknowledgments

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